

# AERODYNAMIC STABILITY OF BRIDGES WITH VARIOUS LEVELS OF STRUCTURAL DAMPING

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## Abstract

**Introduction:** Structural damping is one of the most important parameters affecting the aerodynamic stability of bridge structures. **Purpose of the study:** We aimed to assess the effect that structural damping of a bridge structure has on its stability in a wind current. **Methods:** In the course of the study, we performed experimental studies of the aerodynamic stability in typical girder bridge structures (with two and four main girders) with different levels of structural damping, facilitated by a unique experimental unit: Large Research Gradient Wind Tunnel, courtesy of the National Research Moscow State University of Civil Engineering (NRU MGSU). **Results:** The results of the experimental studies show that, despite the general trend towards the decrease in the amplitude of bridge span structure oscillations as the structural damping level increases, the dependence between these parameters is nonlinear. When providing R&D support in the design of real-life structures, in case it is necessary to increase the aerodynamic stability of the superstructure by increasing the level of structural damping (changing the type of joints in structural elements, using mechanical damping devices), it is recommended to conduct experimental studies in wind tunnels to assess the effectiveness of a given solution.

## Keywords

Bridge structure, structural damping, wind tunnel, experimental studies, sectional model.

## Introduction

In the modern world, experimental studies of the aerodynamic stability of large-span bridge structures are an integral part of bridge design. It is very difficult to overestimate the importance of such studies, given the number of accidents involving bridge structures that occurred due to wind impact (Bas and Catbas, 2021; Maystrenko et al., 2017; Tan et al., 2020). In the Russian Federation, testing in wind tunnels is regulated by the following standards: Regulations SP 35.13330.2011 "Bridges and Culverts" and Regulations SP 296.1325800.2017 "Buildings and Structures. Accidental Actions". The main methods for conducting such studies are full-scale modeling (Argentini et al., 2020; Miyata et al., 1992), studies with sectional models (Cermak, 2003; Diana et al., 2013; Reinhold et al., 1992), as well as numerical modeling in specialized software systems (Ageev et al., 2021; Diana and Omarini, 2020; Li et al., 2017). They are the subject of many works by Russian and foreign researchers, as well as of a number of regulatory documents (Highways England, 2020; National Research Council of Italy. Advisory Committee on Technical Recommendations for Construction, 2008).

Among others, the methodology for conducting experimental studies on dynamically similar sectional

models is described in the scientific, technical, and regulatory literature in most detail and most comprehensively (Poddaeva et al., 2018; Wardlaw, 1980). The main similarity criteria, in this case, are the following: the Cauchy and Newton numbers (correspondence between the model's and the real object's distribution of masses and moments of inertia); the Scruton number (correspondence between the model's and the real object's logarithmic decrement of oscillations); and the Strouhal number (correspondence between the model's and the real object's frequency characteristics).

One of the most significant research insights is the dependence of the bridge span oscillation amplitude on the velocity of the wind flow at different angles of attack.

If experimental studies detect an unlimited increase in the amplitude of oscillations, this is likely to be caused by one of the phenomena of aerodynamic instability found unacceptable under the Regulations SP 35.13330.2011 and SP 296.1325800.2017, namely galloping, divergence or flexural-torsional flutter (Kazakevich, 2021; Solovyev, 2016). In this case, the most effective solution to the problem is to change the wind flow around the superstructure by making changes to the superstructure design (using deflectors, fairings, etc.) (SP 296.1325800.2017; Nagao et al., 1993;

Wardlaw, 1992).

When oscillations have a narrow velocity range (meaning that when the velocity increases, the oscillations stop), we can talk about the appearance of vortex excitation (Kazakevich, 2021). Here, the maximum value of the oscillation amplitude is important; it must be compared with the maximum permissible value of the vertical deflection of the bridge span. Despite the effectiveness of aerodynamic damping methods, in this case, designers often resort to increasing structural damping without changing the shape of the bridge span's cross-section. This can be linked to a change in the design features of the respective structure, such as changing the type of connection from welded to ordinary bolted, which increases the level of structural damping from 0.02 to 0.05. The main question, in this case, is the following: how significant is the drop in the oscillation amplitude going to be? What is even more important to know is the effect that the value of structural damping has on the oscillation amplitude of the bridge span when using different types of mechanical damping devices. The required mass of counterweights and other parameters of additional dampers directly depend on this.

#### Subject, tasks, and methods

As the target of our study, we chose one of the most common types of bridge structures: girder bridges with two and four girders (Figures 1–2).

For the purposes of this study, we used a unique experimental unit, the Large Research Gradient Wind Tunnel by the National Research Moscow State University of Civil Engineering (NRU MGSU), in a specialized test bench for static and dynamic tests of building structures.

The methodology for experimental studies of bridge structures' aerodynamic stability in sectional models is described in detail in the scientific and technical literature (Brownjohn and Choi, 2001; Diana

et al., 2015). The main task of dynamic tests is to determine the amplitude of bridge span oscillations at various wind flow velocities and angles of attack. As measuring equipment, we used the RAS-T contactless laser displacement sensors by WayCon, which are included in the State Register of Measuring Instruments. The flow velocity in the wind tunnel was recorded with a Pitot-Prandtl tube and a differential pressure gauge.

The main requirement for the model is that it must retain geometric similarity and ensure that its distribution of masses and moments of inertia is consistent with the corresponding parameters of the real object (the Cauchy and Newton numbers mentioned in the introduction). Besides, the model must be as rigid as possible. This is necessary to maintain Scruton number similarity since metal spans with welded joints have a specific minimum level of structural damping. The frequency parameters of the real object are modeled with spring suspensions of a specialized test bench (Figure 3). The sensors are aimed at markers located in the corners of the model, making it possible both to determine the amplitude of the oscillations and to classify their mode.

The level of structural damping is measured with the free damped oscillation method. When subjected to a pulsed external load, the model begins to oscillate, while the sensors record its oscillogram (Figure 4). This oscillogram is analyzed in the software package. The rate of oscillation amplitude reduction is determined by the relative dissipation of energy. The corresponding value is the value of the logarithmic decrement.

The level of structural damping was adjusted with the help of special flexible inserts in the spring suspensions of the specialized test bench.

#### Results and discussion

Tables 1–2 show the dynamic parameters of the models obtained during bench tests.

Table 1. Correlations between the model and the real object (Model No. 1)

	Oscillation mode	Real object	Model	Velocity scale U*
Frequencies in the real object and the model	Bending	0.48 Hz	5.22 Hz	6.43
	Torsion	1.33 Hz	9.62 Hz	9.67

Table 2. Correlations between the model and the real object (Model No. 2)

	Oscillation mode	Real object	Model	Velocity scale U*
Frequencies in the real object and the model	Bending	0.596 Hz	6.1 Hz	6.8
	Torsion	1.36 Hz	12.15 Hz	7.8

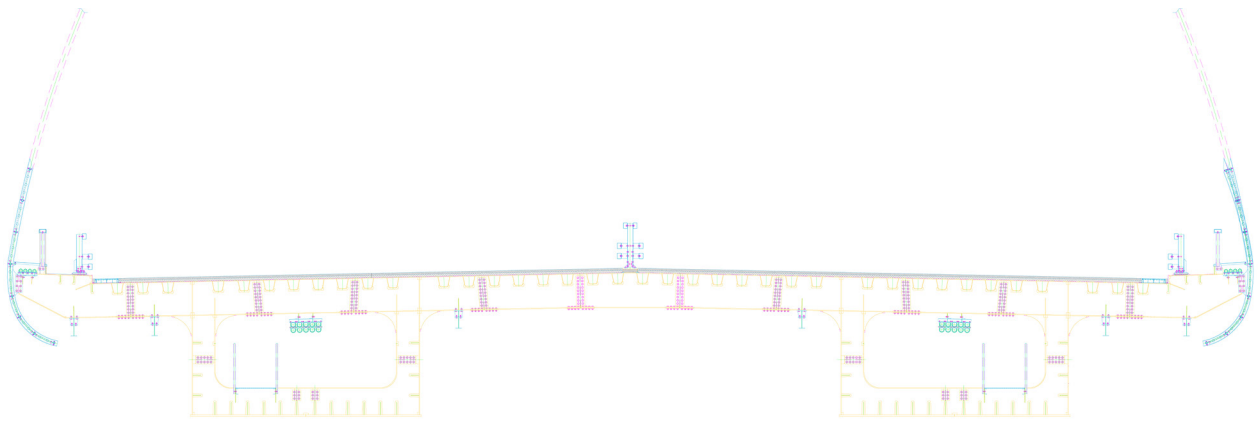


Figure 1. Cross-section of the bridge (Model No. 1)

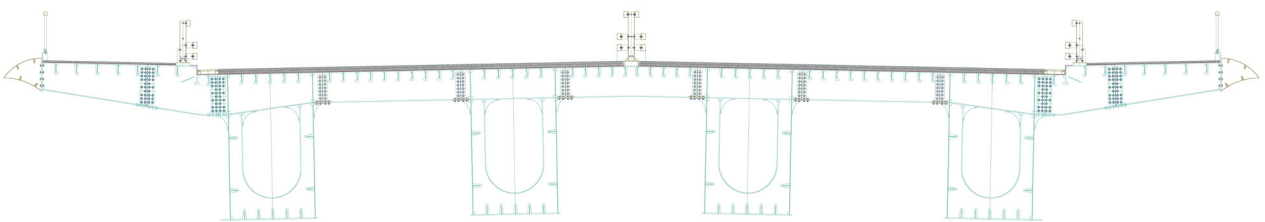


Figure 2. Cross-section of the bridge (Model No. 2)



Figure 3. Spring suspensions of the specialized test bench

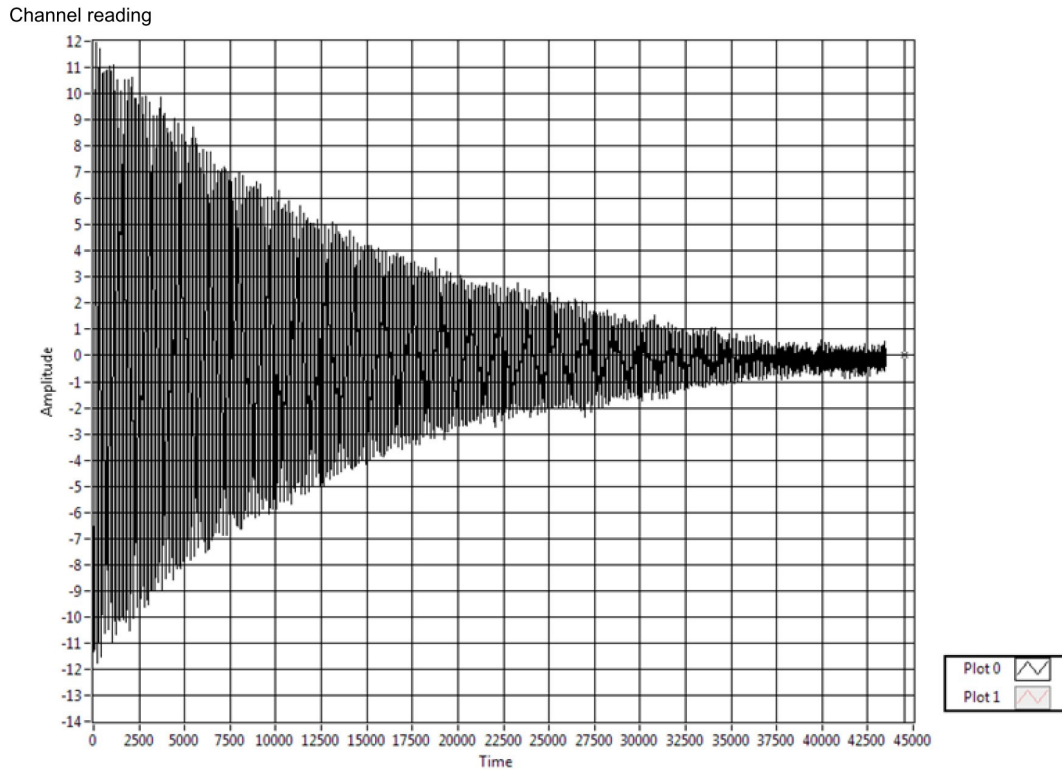


Figure 4. Oscillogram of the model's oscillations

The studies were carried out at the following levels of structural damping: 0.03, 0.045, 0.055, 0.07. The research results are presented as graphs that show the bridge span oscillation amplitude's dependence on the velocity of the wind flow.

As the most illustrative material, we selected those wind flow angles of attack where the phenomenon of span vortex excitation was detected. In this case, the oscillation frequency of the structure corresponds to the natural oscillation frequency recorded at the preliminary stage of the studies (Tables 1–2).

Figures 5–6 show the results for model No. 1 at the following wind flow angles of attack:  $-5^\circ$  (downward flow) and  $+5^\circ$  (upward flow).

Figures 7–8 show the results for model No. 1 at the following wind flow angles of attack:  $-3^\circ$  (downward flow) and  $+3^\circ$  (upward flow).

By analyzing the experimental study results, we obtained the ratio of the increase in structural damping ( $\Delta\delta$ , %) to the corresponding decrease in the maximum oscillation amplitude ( $\Delta A$ , %) for different models at different angles of attack ( $\alpha$ ).

Table 3. Ratio of the increase in structural damping ( $\Delta\delta$ , %) to the corresponding decrease in the maximum oscillation amplitude ( $\Delta A$ , %) for different models at different angles of attack ( $\alpha$ )

Model No. 1						
$\alpha$ , °	-5			5		
$\Delta\delta$ , %	33	45	57	33	45	57
$\Delta A$ , %	12	39	66	17	39	69
Model No. 2						
$\alpha$ , °	-3			3		
$\Delta\delta$ , %	33	45	57	33	45	57
$\Delta A$ , %	6	39	70	19	44	59

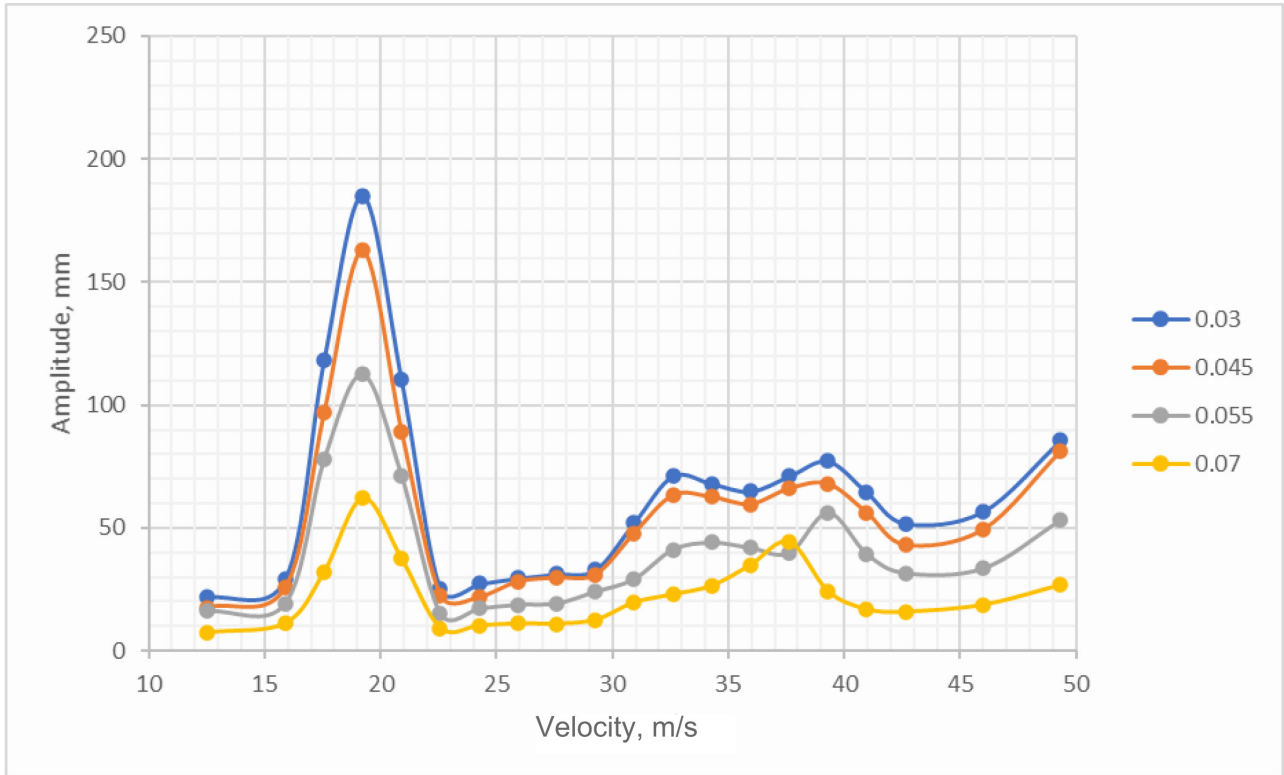


Figure 5. Oscillation amplitude's dependence on the wind flow velocity in the model at an angle of attack of  $-5^\circ$

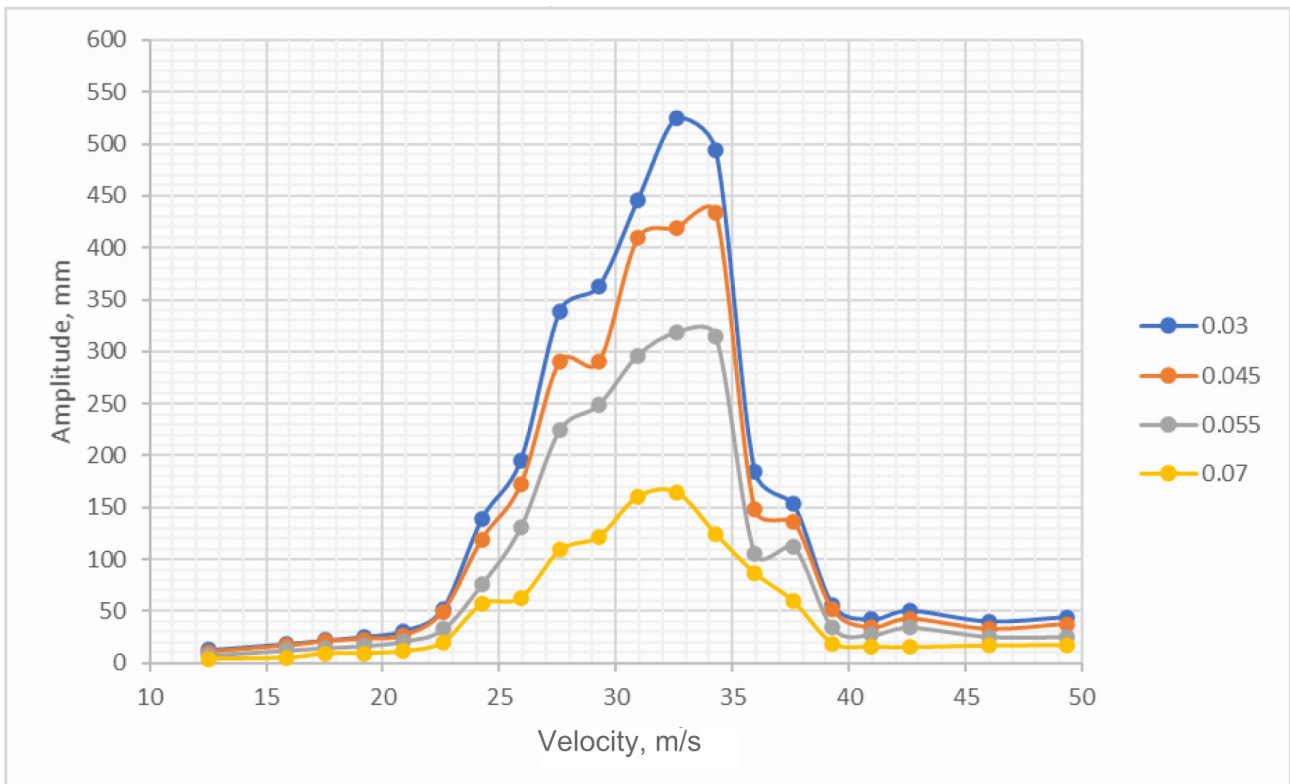


Figure 6. Oscillation amplitude's dependence on the wind flow velocity in the model at an angle of attack of  $+5^\circ$

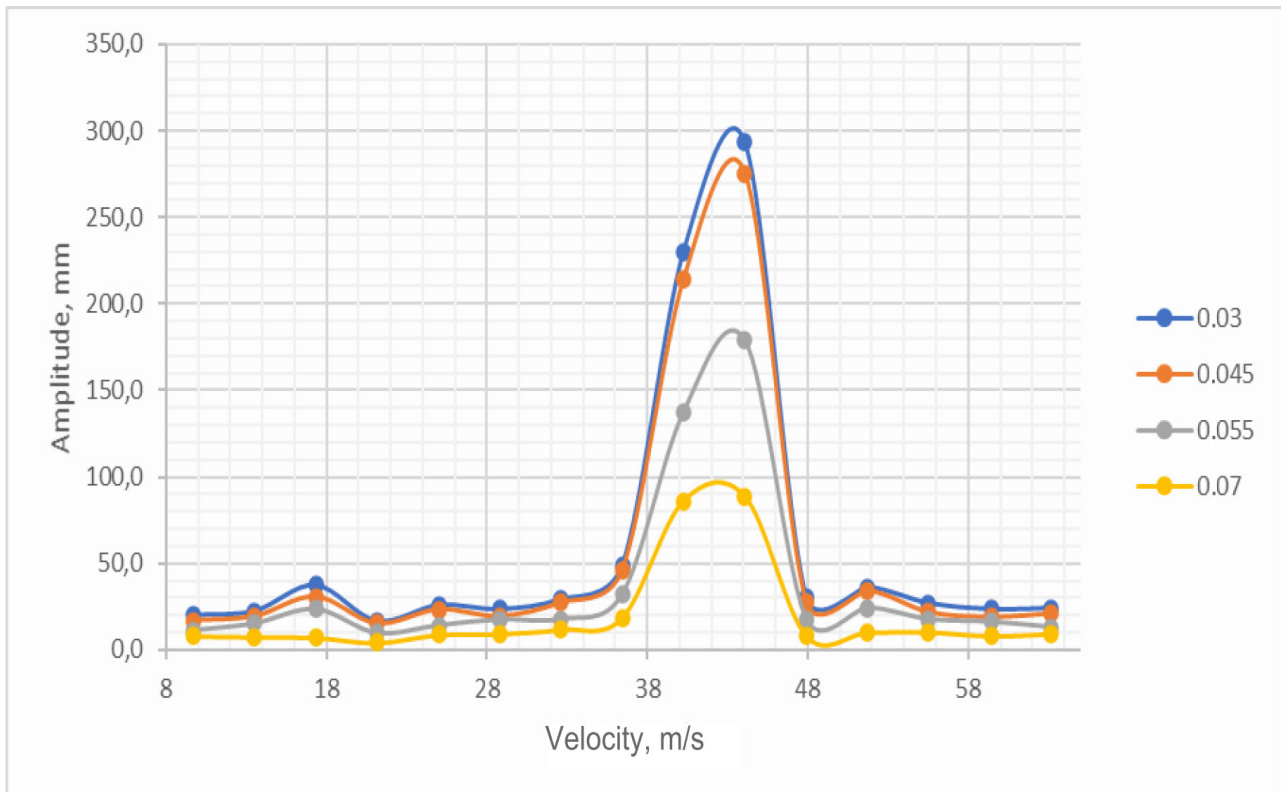


Figure 7. Oscillation amplitude's dependence on the wind flow velocity in the model at an angle of attack of  $-3^\circ$

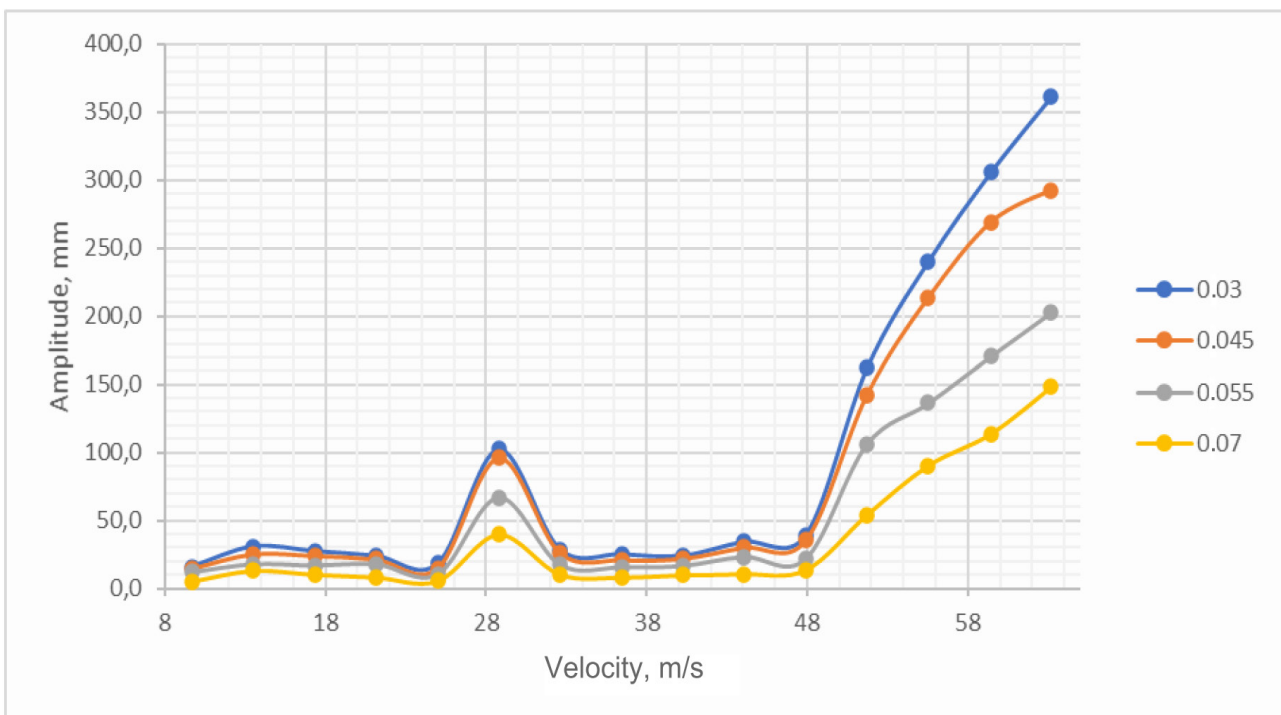


Figure 8. Oscillation amplitude's dependence on the wind flow velocity in the model at an angle of attack of  $+3^\circ$

### Conclusions

The results obtained show that, despite the general trend towards the decrease in the amplitude of bridge span structure oscillations as the structural damping level increases, the dependence between these parameters is nonlinear.

When increasing the aerodynamic stability of large-span bridge structures by means of increasing the structural damping level, it is necessary to make appropriate engineering calculations and thus determine the expected value of the oscillations' logarithmic decrement after making structural

changes. We further recommend conducting additional experimental studies in a wind tunnel in order to assess the effectiveness of the solution selected.

Compliance with these requirements will help both to ensure the reliability and safety of bridge structures and to optimize the costs of increasing structural damping.

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## АЭРОДИНАМИЧЕСКАЯ УСТОЙЧИВОСТЬ МОСТОВ С РАЗЛИЧНЫМИ УРОВНЯМИ СТРУКТУРНОГО ДЕМПФИРОВАНИЯ

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### Аннотация

Конструкционное демпфирование является одним из наиболее важных параметров, влияющих на аэродинамическую устойчивость мостовых сооружений. **Цель исследования:** Оценка влияния конструкционного демпфирования мостовой конструкции на ее устойчивость в ветровом потоке. **Методы:** Экспериментальные исследования аэродинамической устойчивости типовых балочных мостовых сооружений (с двумя и четырьмя главными балками) с различными уровнями конструкционного демпфирования на базе Уникальной научной установки «Большая исследовательская градиентная аэродинамическая труба» НИУ МГСУ. **Результаты:** На основании результатов проведенных экспериментальных исследований, установлено, что несмотря на общую тенденцию снижения амплитуды колебаний пролетного строения мостового сооружения с увеличением уровня конструкционного демпфирования, зависимость этих параметров имеет нелинейный характер. При проведении научно-технического сопровождения проектирования реальных сооружений, в случае необходимости повышения аэродинамической устойчивости пролетного строения путем повышения уровня конструкционного демпфирования (изменение типа соединений конструктивных элементов, использование механических демпфирующих устройств), рекомендуется проведение экспериментальных исследований в аэродинамических трубах для оценки эффективности того или иного решения.

### Ключевые слова

Мостовое сооружение, конструкционное демпфирование, аэродинамическая труба, экспериментальные исследования, секционная модель.